

## SEMICONDUCTOR LASER DRIVE CIRCUIT AND PHOTOELECTRIC SENSOR

## BACKGROUND OF THE INVENTION

## 1. Field of the invention

**[0001]** The present invention relates to a semiconductor laser drive circuit and a photoelectric sensor provided with the circuit.

## 2. Description of the related art

**[0002]** Photoelectric sensors of the light transmission type generally comprise a light emitting element and a light receiving or detecting element both opposed to each other. Laser beams emitted by the light emitting element are blocked by an object when the object is placed in the middle of a light path from the light emitting element to the light receiving element. An amount of light received by the light receiving element varies depending upon the presence or absence of an object in the middle of the light path. Thus, the presence or absence of the object is detected, or the position or dimensions of the object are measured on the basis of variations in the amount of light received by the light receiving element of the photoelectric sensor. In order that the photoelectric sensor may perform a stable detection or measurement, output of the light emitting element is required to be constant.

**[0003]** For the purpose of obtaining a constant output, a semiconductor laser drive circuit has conventionally been provided in the photoelectric sensor. The semiconductor laser drive circuit carries out an automatic power control (APC) to control the light emitting element so that output of the element is rendered constant.

The semiconductor laser drive circuit includes a laser diode serving as the foregoing light emitting element and a monitor photodiode mounted in the same chip along with the mounted laser diode. An amount of electric current flowing into the monitor photodiode changes in response to an amount of light emitted by the laser diode. A feedback control loop is carried out on the basis of an amount of current flowing into the monitor photodiode so that the output level of the laser diode maintains a predetermined intensity.

**[0004]** In one type of the laser diode having a built-in monitor photodiode, a cathode of the laser diode and an anode of the monitor photodiode are connected in common. Recently, however, another type of laser diode has appeared in which cathodes of both diodes are connected in common has mainly been used. This type is often referred to as a "cathode common connection type." The laser diode of the cathode common connection type commonly available at low costs due to the benefits of mass production.

**[0005]** FIGS. 4A and 4B illustrate arrangements of conventional semiconductor laser drive circuits employing laser diodes of the cathode common type respectively. JP-A-61-202345 and Japanese Patent No. 2540850 disclose semiconductor laser drive circuits of the cathode common connection type.

**[0006]** In the laser diode of the cathode common connection type, the cathodes of the laser diode 1 and monitor photodiode 2 are connected in common as described above. Accordingly, the cathodes are connected in common to a ground line 3 in the circuit as shown in FIG. 4A. Furthermore, the laser diode 1 is connected between the ground line 3 and a positive power supply 4, whereas the monitor photodiode 2

is connected between the ground line 3 and a negative power supply 5. Thus, the circuit shown in FIG. 4A requires two power supplies 4 and 5, which complicates a power supply circuit and increases a mounting or packaging area. The requirement of the two power supplies limits potential reduction in the size of the overall device and results in a cost increase.

**[0007]** On the other hand, in the circuit shown in FIG. 4B, only the positive power supply 4 is used without the negative power supply. However, no reverse voltage is applied to the monitor photodiode 2 and accordingly, the photodiode is unbiased. Consequently, even when the monitor photodiode 2 receives or detects light, a linear current flow does not respond quickly to the detection. This results in a delay in the build-up of load voltage of a resistor 6 connected in parallel to the monitor photodiode 2. Accordingly, a high-speed APC cannot be realized in the circuit shown in FIG. 4B.

#### SUMMARY OF THE INVENTION

**[0008]** Therefore, an object of the present invention is to provide a semiconductor laser drive circuit that is a drive circuit for a semiconductor laser element. Components of the semiconductor laser element could include a semiconductor laser drive diode and a monitor photodiode both having their respective cathodes connected in common. In addition, an object of the present invention is to provide a semiconductor laser drive circuit that can realize a high-speed control with use of a single power supply. A further object includes, but is not limited to, a photoelectric sensor provided along with the

semiconductor laser drive circuit.

**[0009]** To achieve the various objects identified and others not identified, the present invention provides a semiconductor laser drive circuit for a semiconductor laser element including a semiconductor laser drive diode and a monitor photodiode both having respective cathodes connected in common, wherein the semiconductor laser diode has an anode connected to a power supply line side and the monitor photodiode has an anode connected to a ground line side via a voltage generating unit generating voltage according to an amount of current flowing into the monitor photodiode. The semiconductor laser drive circuit comprises a current control element adjusting an amount of current supplied to the semiconductor laser diode, a feedback control unit receiving a voltage generated by the voltage generating element to supply a control signal to a control terminal of the current control element based upon the relationship of a reference voltage level to the voltage generated, thereby controlling in a feedback manner the output laser beam of the semiconductor laser diode so as to maintain the output laser beam at a predetermined level, and a biasing element provided between the common cathode connections of the semiconductor laser diode and the monitor photodiode, and the ground line, the biasing element applying a reverse bias voltage to the monitor photodiode.

**[0010]** When the light receiving unit receives light emitted by the light emitting unit, a current relating to an amount of received light flows into the monitor photodiode. The voltage generating element may then generate a voltage with a level corresponding to the amount of current. The feedback control unit may deliver a control signal to the current control element proportionate to the generated

voltage level . The delivered control signal may be one corresponding to a difference between the level of voltage generated by the voltage generating element and a reference voltage level corresponding to a known laser output level of the semiconductor laser diode, for example. Consequently, the laser light output of the semiconductor laser diode may be controlled to correspond to a predetermined level (the aforesaid known laser output level).

**[0011]** In the above-described semiconductor laser drive circuit, the laser light output of the semiconductor laser diode can be controlled in the feedback manner with the use of a single power supply. Furthermore, since the biasing element applies the reverse bias voltage (reverse voltage) to the monitor photodiode, current flowing into the monitor photodiode can be rendered linear relative to variations in an amount of light received by the monitor light receiving element. Consequently, a high-speed feedback control loop can be realized.

**[0012]** In a preferred form, the current control element is connected in series between the cathode connection of the semiconductor laser diode and the monitor photodiode, and the biasing element. In this arrangement, only the current control element and semiconductor laser diode can be connected between the biasing element (examples include but are not limited to a resistor or Zener diode) and the power supply line. Consequently, since a high level voltage corresponding to a load voltage of the aforesaid resistor is applied as the reverse bias voltage to the monitor photodiode, current levels flowing into the monitor photodiode can respond quickly to variations in light detected or received by the photodiode.

**[0013]** The present invention also provides a photoelectric sensor

comprising a light emitting unit emitting light directed to a predetermined detection region and a light receiving unit receiving light from the detection region, thereby performing a detecting operation according to a level of the light received by the receiving unit, the light emitting unit including a semiconductor laser drive circuit for a semiconductor laser element including a semiconductor laser drive diode and a monitor photodiode both having respective cathodes connected in common, wherein the semiconductor laser diode has an anode connected to a power supply line side and the monitor photodiode has an anode connected to a ground line side via a voltage generating unit generating voltage according to an amount of current flowing into the monitor photodiode. The semiconductor laser drive circuit comprises a current control element adjusting an amount of current supplied to the semiconductor laser diode, a feedback control unit receiving a voltage generated by the voltage generating element to supply a control signal to a control terminal of the current control element based upon the relationship of a reference voltage level to the voltage generated, thereby controlling in a feedback manner the output laser beam of the semiconductor laser diode so as to maintain the output laser beam at a predetermined level, and a biasing element provided between the common cathode connection of the semiconductor laser diode and the monitor photodiode, and the ground line, the biasing element applying a reverse bias voltage to the monitor photodiode.

**[0014]** The foregoing semiconductor laser drive circuit can be employed in the photoelectric sensor. Consequently, the semiconductor laser diode can be controlled at a higher speed, and with a lower response time in the detection or measurement of an

object. Furthermore, the size of the photoelectric sensor can be reduced beyond that of a photoelectric sensor in which two power supplies have been used.

#### BRIEF DESCRIPTION OF THE DRAWINGS

**[0015]** Other objects, advantages and features of the present invention will become clear upon reviewing the following description of embodiment, made with reference to the accompanying drawings, in which:

FIG. 1 illustrates an overall construction of a photoelectric sensor in accordance with an embodiment of the present invention;

FIG. 2 is a schematic circuit diagram of the semiconductor laser drive circuit in accordance with the present invention;

FIG. 3 is a circuit diagram of the semiconductor laser drive circuit in accordance with another embodiment of the invention; and

FIGS. 4A and 4B are circuit diagrams of conventional two power source and one power source common cathode connection type semiconductor laser drive circuits respectively.

#### DETAILED DESCRIPTION OF THE INVENTION

**[0016]** An embodiment of the present invention will be described with reference to FIGS. 1 and 2. A transmittance photoelectric sensor 10 of the embodiment includes a light emitting section 11 having a rectangular slit-like emitting window 12 from which parallel rays of light are emitted and a light receiving section 21 also having

a rectangular slit-like light receiving window 22. The light emitting section 11 and the light receiving section 21 are disposed to be opposed to each other. Light emitted from the light emitting window 12 of the light emitting section 11 impinges into the light receiving window 22 of the light receiving section 21. A light path between the windows 12 and 22 is set as a detectable region R1 for the photoelectric sensor 10. The region R1 is defined by broken lines in FIG. 1. When an object is present in the region R1, light emitted from the light emitting window 12 is blocked by the object. An amount of light received by the light receiving section 21 varies depending upon a degree of blocking. For example, dimensions of the object are measured on the basis of an amount of light received by the light receiving section 21.

**[0017]** The light emitting section 11 comprises a light emitting case 13, a semiconductor chip 14 serving as a semiconductor laser element in the invention and a light emitting lens 15 disposed in front of the semiconductor chip. The semiconductor chip 14 includes a laser diode 30 and a monitor photodiode 31 both enclosed in the same package. The laser diode 30 and the monitor photodiode 31 have respective cathodes connected in common. The lens 15 is, for example, a thick semicircular plate-shaped concavoconvex lens. The lens 15 is disposed so that a convex portion thereof is located at the light emitting window 12 side. The lens 15 converts radially spread light emitted by the laser diode 30 to the parallel rays traveling to the opposed light receiving section 21 side. The light emitting case 13 includes a wall located in front of the lens 15 and formed with a slit-like opening which is closed by a light transmitting member



12a such as glass, whereby the light emitting window 12 is formed.

**[0018]** The light receiving section 21 comprises a light receiving case 23, a light receiving or detecting element 24 and a light receiving lens 25 converging the parallel rays from the light emitting section 11. The light receiving case 23 also includes a wall located in front of the lens 25 and formed with a slit-like opening which is closed by a light transmitting member 22a such as glass, whereby the light emitting window 22 is formed. The light emitting and receiving sections 11 and 21 are disposed to be opposed to each other while long axes correspond with each other.

**[0019]** The semiconductor laser drive circuit will now be described. The laser light output of the laser diode 30 needs to be maintained at a constant value in order that the transmittance photoelectric sensor 10 may perform a stable detection or measurement. For this purpose, a semiconductor laser drive circuit 26 is provided. Referring to FIG. 2, reference numeral 14 designates the aforesaid semiconductor chip. The laser diode 30 has an anode connected to a power supply line L1 and a cathode to which a collector of an NPN transistor 32 is connected. The cathodes of the monitor photodiode 31 and the laser diode 30 are connected to a common node. The NPN transistor 32 serves as a current control element in the invention. The NPN transistor 32 has an emitter connected via an emitter resistor 33 to a ground line G. The emitter resistor 33 serves as a biasing element in the invention. The NPN transistor 32 further has a base connected to an output terminal of a differential amplifier 34. The NPN transistor 32 controls an amount of current flowing into the laser diode 30 according to a level of control signal delivered from the

differential amplifier 34.

**[0020]** The monitor photodiode 31 has an anode connected via a resistor 35 to the ground line G. Load voltage of the resistor 35 takes a value according to an amount of current flowing into the monitor photodiode 31. Accordingly, the resistor 35 serves as a voltage generating unit in the invention. The resistor 35 will hereinafter be referred to as "current detecting resistor." A voltage level  $V_r$  at a node of the resistor 35 and the monitor photodiode 31 is supplied to one input of the differential amplifier 34. The other input of the differential amplifier 34 is connected via a resistor 36 to the power supply line L1, whereby a predetermined reference voltage level  $V_{ref}$  is supplied to said other input of the differential amplifier. Thus, the differential amplifier 34 supplies, to the base of NPN transistor 32, a control signal with a level according to the difference between the aforesaid reference voltage level  $V_{ref}$  and the voltage level  $V_r$  varying according to the current flowing into the monitor photodiode 31.

**[0021]** The above-described semiconductor laser drive circuit 26 operates as follows. When a positive power supply voltage level  $V_{cc}$  is applied to the power supply line L1, the voltage level  $V_r$  applied to the input of the differential amplifier 34 is lower than the reference level  $V_{ref}$  since the monitor photodiode 31 receives no light from the laser diode 30 at an initial stage. Accordingly, the voltage level at the base of the NPN transistor 32 (hereinafter, "base voltage level  $V_b$ ") is high so that the NPN transistor is turned on. A corresponding amount of current flows into the laser diode 30, so that the laser diode emits light. Since current also flows into the emitter resistor

33 in this case, the emitter voltage level  $V_e$  of the NPN transistor 32 becomes substantially equal to a voltage level obtained by subtracting a voltage drop  $V_d$  across the laser diode 30 from the power supply voltage level ( $V_{cc} - V_d$ ). The emitter voltage level  $V_e$  is supplied to the monitor photodiode 31 and current detecting resistor 35. In other words, a reverse bias voltage (reverse voltage) is applied to the monitor photodiode 31. The level of this reverse bias voltage varies during the APC. However, an amount of current flowing from the diode 30 to the photodiode 31 is smaller than an amount of current flowing into the NPN transistor 32. Consequently, an amount of current according to an amount of light received by the photodiode 31 can be supplied to the current detecting resistor 35 serving as the voltage generating element without adverse effect of variations in the aforesaid reverse bias voltage. In short, the voltage level  $V_r$  is barely adversely affected by the variations in the reverse bias voltage level.

**[0022]** On the other hand, the monitor photodiode 31 receives light emitted by the laser diode 30. An amount of current according to an amount of received light flows into the photodiode 31. Since the reverse bias voltage is applied to the photodiode 31, the amount level of current flowing into the photodiode 31 quickly rises upon receipt of light. The current amount level thereafter varies in a linear mode relative to the variations in the amount of received light. This voltage level  $V_r$  varying in the linear mode relative to the variations in the amount of received light is supplied to the input of the differential amplifier 34.

**[0023]** An amount of light received by the photodiode 31 is increased

as the laser light output of the laser diode 30 becomes higher. When the difference between the voltage level  $V_r$  and the reference voltage level  $V_{ref}$  becomes smaller, the level of the control signal delivered from the differential amplifier 34 drops and accordingly, the base voltage level  $V_b$  of the NPN transistor 32 drops. As a result, an amount of current flowing into the laser diode 30 is decreased. Conversely, when an amount of light emitted by the laser diode 30 is reduced, the difference between the voltage level  $V_r$  and the reference voltage level  $V_{ref}$  becomes larger, so that the base voltage level  $V_b$  of the NPN transistor 32 is increased. As a result, an amount of current flowing into the laser diode 30 is also increased. Consequently, the output of the laser diode 30 can be maintained at the set level corresponding to  $V_{ref}$ .

**[0024]** In the above-described embodiment, the APC can be carried out with use of a single power supply even when the semiconductor chip 14 of the cathode common type includes the laser diode 30 and the monitor photodiode 31 with their respective cathodes connected in common. Moreover, since the reverse bias voltage is applied to the monitor photodiode 31, linear current can quickly be supplied to the photodiode 31 corresponding to the variations in the amount of light emitted by the laser diode 30 and the variations in the amount of light received by the monitor photodiode 31, as compared with the a circuit arrangement in the aforesaid unbiased state. Consequently, a higher-speed feedback control can be realized with the biasing element.

**[0025]** In the above-described embodiment, only the NPN transistor 32 and laser diode 30 are connected between the emitter resistor 33

(as the biasing element) and the power supply line L1. Accordingly, a high voltage level corresponding to the load voltage of the emitter resistor 33 is applied as the reverse bias voltage to the monitor photodiode 31. Consequently, allowing the current flowing into the photodiode 31 to respond more quickly than without the reverse bias voltage.

**[0026]** Furthermore, when the above-described semiconductor laser drive circuit is employed in the transmittance photoelectric sensor 10, a high-speed control of the laser diode 30 can be realized and accordingly, a response time in the detection or measurement of the object can be reduced. Furthermore, the size of the light emitting section 11 and the size of the overall photoelectric sensor 10 can be smaller than in comparison to an arrangement in which two power supplies have been used.

**[0027]** FIG. 3 illustrates another embodiment of the invention. One difference between the second embodiment and the previous one is that a PNP transistor 40 is employed as the current control element, instead of the NPN transistor 32, respectively. Furthermore, the configuration of the biasing element is different than the configuration of biasing element presented in the first embodiment.

**[0028]** Referring to FIG. 3, the PNP transistor 40 (serving as a current control element) is connected between the power supply line L1 and the anode of the laser diode 30. A resistor 41 is connected in series to a Zener diode 42 between the power supply line L1 and the ground line G. The cathodes of the laser diode 30 and the monitor photodiode 31 are connected to the node between the resistor 41 and the Zener diode 42. As the result of this arrangement, voltage applied

to the Zener diode 42 is applied as the reverse bias voltage to the monitor photodiode 31 to which the Zener diode is connected in parallel.

**[0029]** In the second embodiment, the APC control can also be carried out with use of a single power supply even when the semiconductor chip 14 of the cathode common type is employed. Moreover, since the reverse bias voltage is applied to the monitor photodiode 31, a high-speed feedback control, as compared to non-biased configurations, can be realized.

**[0030]** Furthermore, when the above-described semiconductor laser drive circuit 26 is provided in the transmittance type photoelectric sensor 10, a high-speed control of the laser diode 30 can be realized and accordingly, a response time in the detection or measurement of the object can be reduced. Furthermore, the size of the light emitting section 11 and the size of the overall photoelectric sensor 10 can be rendered smaller than in an arrangement in which two power supplies have been used.

**[0031]** Several modified forms will be described, but not limited to the following. The semiconductor laser drive circuit 26 is described as applied to the transmittance type photoelectric sensor 10 in the foregoing embodiments. However, the semiconductor laser drive circuit 26 may also be applied to reflection type photoelectric sensors as well. Additionally, the semiconductor laser drive circuit 26 may be applied to optical pickup devices such as those currently provided in compact disc (CD) players and digital versatile disc (DVD) players as well as bar code readers/scanners.

**[0032]** The resistor 36 may be replaced with a variable resistor in each of the foregoing embodiments. In such a situation, the

reference voltage level  $V_{ref}$  can be varied so that the resulting level of output of the laser diode 30 is modified. Furthermore, the emitter resistor 33 may also be replaced with a variable resistor in the first embodiment so that the speed of the APC can be adjusted and/or optimized. Additionally, the bipolar transistor is used as the current control element in each embodiment. However, a field-effect transistor (FET) may be used in place of the bipolar transistor as the current control element.

**[0033]** The foregoing description and drawings are merely illustrative of the principles of the present invention and are not to be construed in a limiting sense. Various changes and modifications will become apparent to those of ordinary skill in the art. All such changes and modifications are seen to fall within the scope of the invention as defined by the appended claims.